

Lateral Earth Pressure

# Rekayasa Pondasi II

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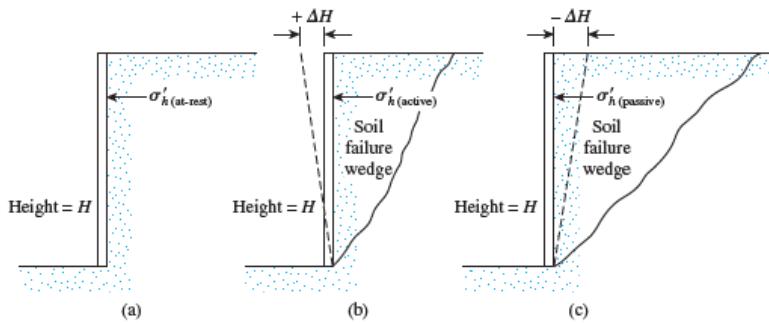
## Lateral Earth Pressure

### Introduction

Kemiringan mendekati vertikal biasanya akan ditopang oleh *Retaining wall*, *cantilever sheet-pile walls*, *sheet-pile with anchore*, atau struktur lainnya. Desain dari struktur ini memerlukan perkiraan tegangan tanah lateral (*lateral earth pressure*), yang terdiri atas beberapa fungsi faktor seperti :

- (a) Tipe pergerakan struktur
- (b) Parameter kuat geser tanah
- (c) Berat satuan tanah
- (d) Kondisi air tanah di timbunan

# Lateral Earth Pressure



**Figure 12.1** Nature of lateral earth pressure on a retaining wall

- (a) **At-rest earth pressure**: Tidak dizinkan mengalami pergerakan lateral.
- (b) **Active earth pressure**: Dinding miring menjauhi tanah tertahan. Area irisan segitiga kemungkinan akan mengalami *fail*.
- (c) **Passive earth pressure**: Dinding ter dorong menuju tanah yang tertahan yang cukup membuat pergerakan di dinding. Irian tanah segitiga ini akan *fail* juga.

## Lateral Earth Pressure at Rest

### Lateral Earth Pressure at Rest

If the wall is at rest and is not allowed to move at all, either away from the soil mass or into the soil mass, the lateral pressure at a depth  $z$  is:

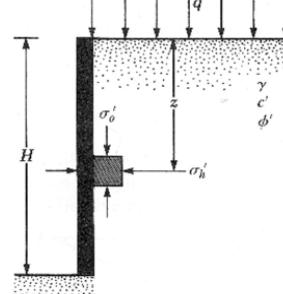
$$\sigma_h = K_o \sigma'_o + u$$

where  $u$  = pore water pressure

$K_o$  = coefficient of at-rest earth pressure

For normally consolidated soil, the relation for  $K_o$  (Jaky, 1944):

$$K_o \approx 1 - \sin \phi'$$
 where  $\phi'$  = drained peak friction angle



For normally consolidated clay, the coefficient of earth pressure at rest can be approximated (Broker and Ireland, 1965) as:

$$K_o \approx 0.95 - \sin \phi'$$

$$K_o = 0.4 + 0.007 (\text{PI}) \quad (\text{for PI between 0 and 40})$$

$$K_o = 0.64 + 0.001 (\text{PI}) \quad (\text{for PI between 40 and 80})$$

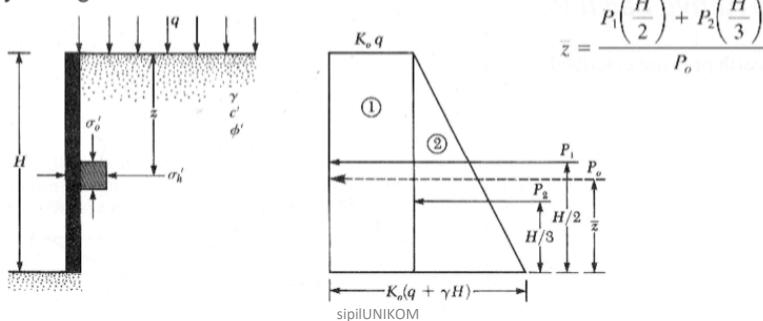
# Lateral Earth Pressure at Rest

For overconsolidated clays:  $K_o(\text{overconsolidated}) \approx K_o(\text{normally consolidated}) \sqrt{\text{OCR}}$

where OCR = overconsolidation ratio

The total force,  $P_o$ , per unit length of the wall can be obtained from the area of the pressure diagram:  $P_o = P_1 + P_2 = qK_oH + \frac{1}{2}\gamma H^2 K_o$

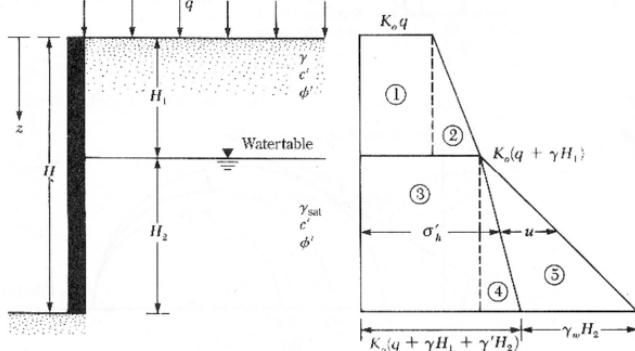
The location of the line of action of resultant force,  $P_o$ , can be obtained by taking moment about the bottom of the wall:



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# Lateral Earth Pressure at Rest

If the water table is located at a depth  $z < H$ , the at rest pressure diagram:



Specifically,  $P_o = A_1 + A_2 + A_3 + A_4 + A_5$

$$P_o = K_o q H_1 + \frac{1}{2} K_o \gamma H_1^2 + K_o(q + \gamma H_1) H_2 + \frac{1}{2} K_o \gamma' H_2^2 + \frac{1}{2} \gamma_w H_2^2$$

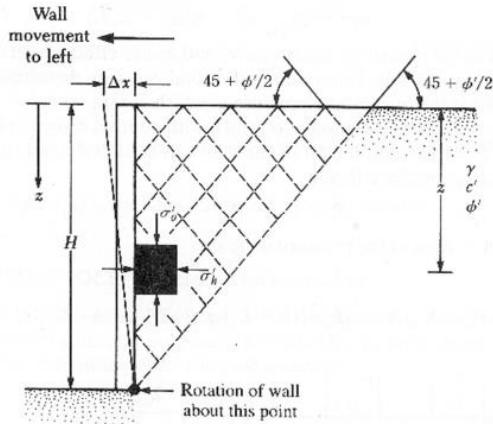
# Lateral Active Earth Pressure

The rankine active pressure  $\sigma_a'$ :

$$\begin{aligned}\sigma_a' &= \sigma'_o \tan^2\left(45 - \frac{\phi'}{2}\right) - 2c' \tan\left(45 - \frac{\phi'}{2}\right) \\ &= \sigma'_o K_a - 2c' \sqrt{K_a}\end{aligned}$$

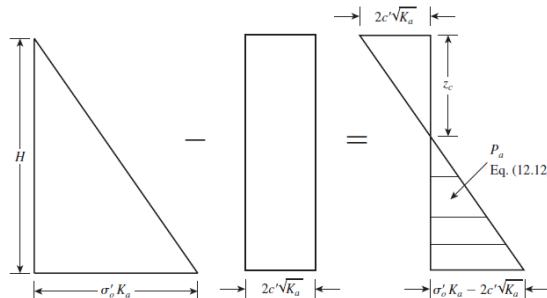
where  $K_a = \tan^2(45 - \phi'/2)$

= Rankine active pressure coefficient



# Lateral Active Earth Pressure

The variation of the active pressure with depth for the wall shown in figure:



The pressure indicating a tensile stress that decrease with depth and becomes zero at a depth  $z = z_c$  or:  $\gamma z_c K_a - 2c' \sqrt{K_a} = 0 \Rightarrow z_c = \frac{2c'}{\gamma \sqrt{K_a}}$

The depth  $z_c$  is usually referred to as the depth of tensile crack, because the tensile stress in the soil will eventually cause a crack along the soil-wall interface.

# Lateral Active Earth Pressure

## Rankine Active Earth Pressure

The total Rankine active force per unit length of the wall before the tensile crack occurs:

$$P_a = \frac{1}{2}\gamma H^2 K_a - 2c' H \sqrt{K_a}$$

After the tensile crack appears, the force per unit length on the wall will be caused only by the pressure distribution between depth  $z = z_c$  and  $z = H$ . This force may be expressed as:

$$P_a = \frac{1}{2}(H - z_c)(\gamma H K_a - 2c' \sqrt{K_a})$$

$$P_a = \frac{1}{2} \left( H - \frac{2c'}{\gamma \sqrt{K_a}} \right) \left( \gamma H K_a - 2c' \sqrt{K_a} \right)$$

# Lateral Passive Earth Pressure

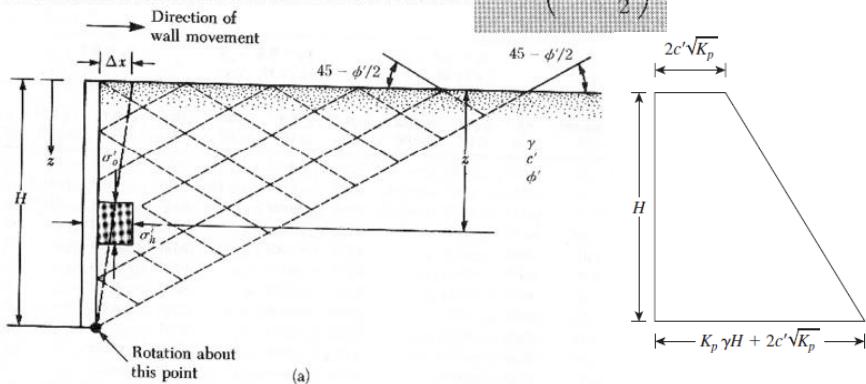
The rankine passive pressure  $\sigma'_p$ :

$$\sigma'_p = \sigma'_p K_p + 2c' \sqrt{K_p}$$

$$\sigma'_p = \gamma H K_p + 2c' \sqrt{K_p}$$

$K_p$  – Rankine passive earth pressure coefficient

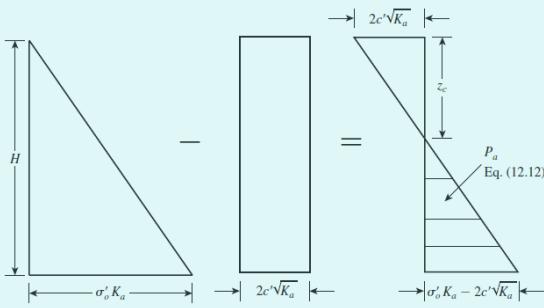
$$= \tan^2 \left( 45 + \frac{\phi'}{2} \right)$$



# Comparation

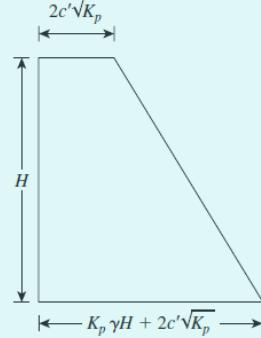
## Active Earth Pressure

$$K_a = \tan^2 \left( 45 - \frac{\phi'}{2} \right)$$



## Passive Earth Pressure

$$K_p = \tan^2 \left( 45 + \frac{\phi'}{2} \right)$$

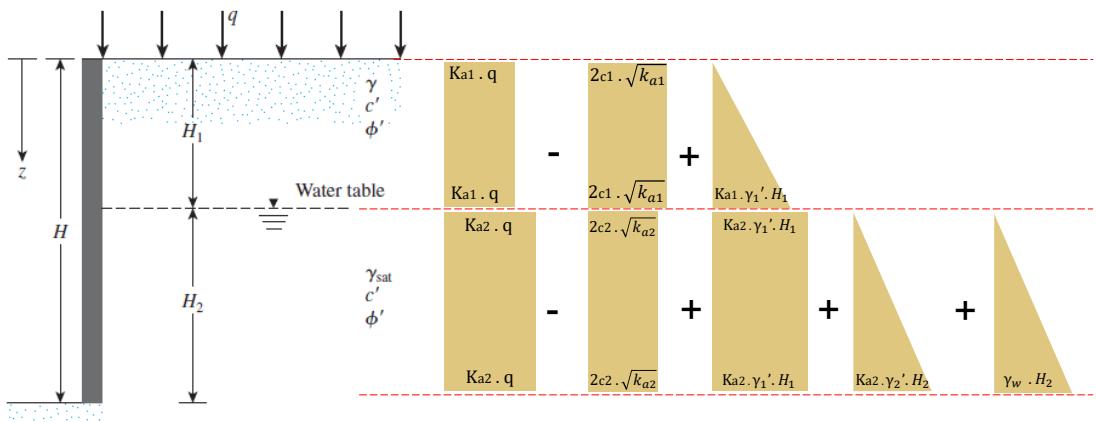


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# Lateral Active Earth Pressure

**Active Earth Pressure**  $K_a = \tan^2 \left( 45 - \frac{\phi'}{2} \right)$



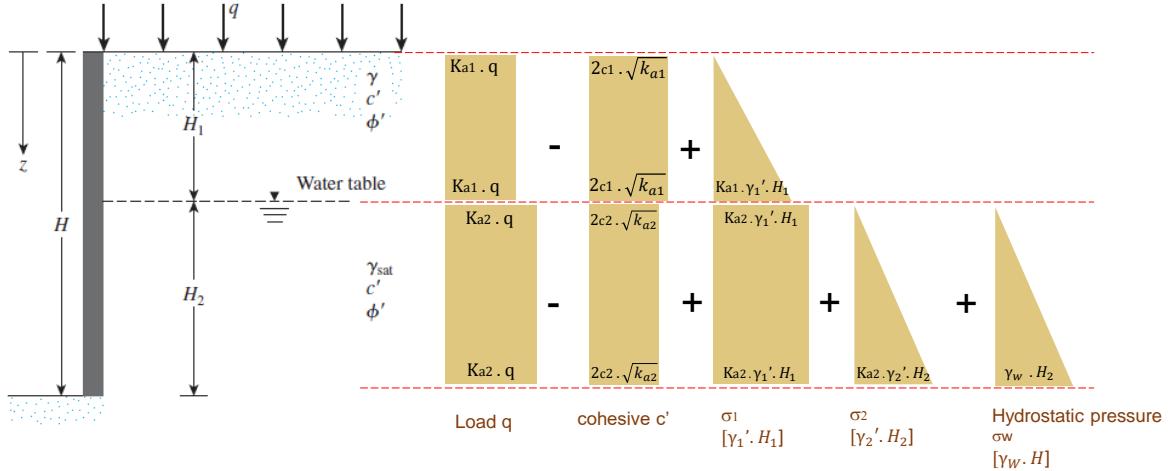
In condition :  
 $\phi_1$  is greater than  $\phi_2$   
 $c_1$  is greater than  $c_2$

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# Lateral Active Earth Pressure

**Active Earth Pressure**  $K_a = \tan^2\left(45 - \frac{\phi'}{2}\right)$

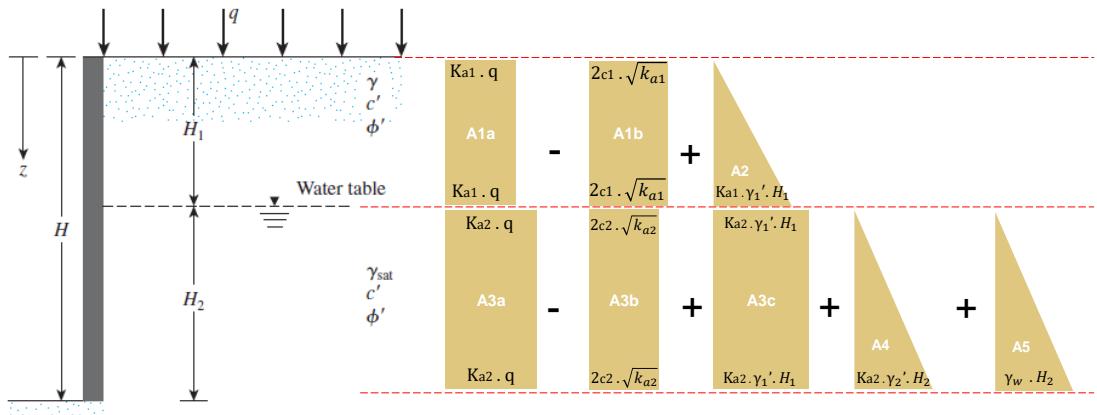


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# Lateral Active Earth Pressure

**Active Earth Pressure**  $K_a = \tan^2\left(45 - \frac{\phi'}{2}\right)$



For summation of the horizontal force :

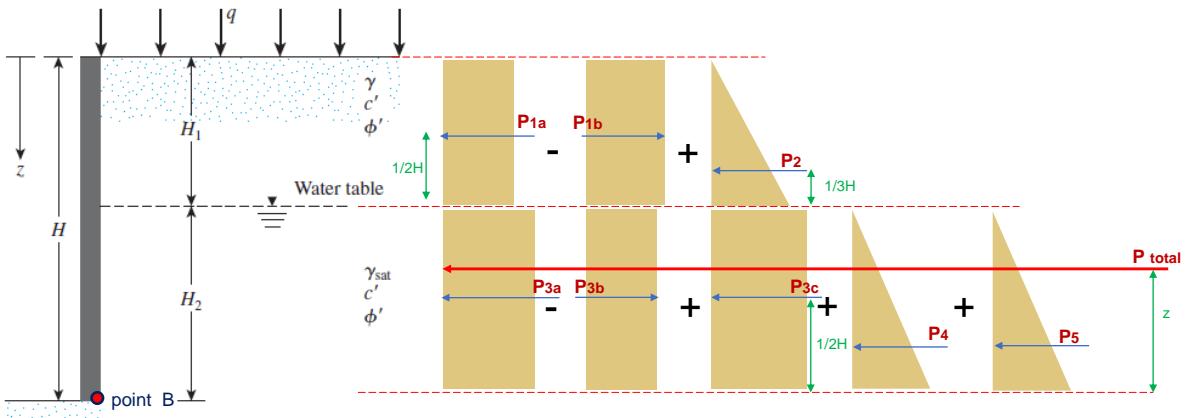
$$P_{total} = A1ab + A2 + A3abc + A4 + A5$$

$$P_{total} = H_1 \cdot (K_{a1} \cdot q - 2c_1 \sqrt{k_{a1}}) + \frac{1}{2} H_1 \cdot (K_{a1} \cdot \gamma'_1 \cdot H_1) + H_2 \cdot (K_{a2} \cdot q - 2c_2 \sqrt{k_{a2}} + K_{a2} \cdot \gamma'_1 \cdot H_1) + \frac{1}{2} H_2 \cdot (K_{a2} \cdot \gamma'_2 \cdot H_2) + \frac{1}{2} H_2 \cdot (\gamma_w \cdot H_2)$$

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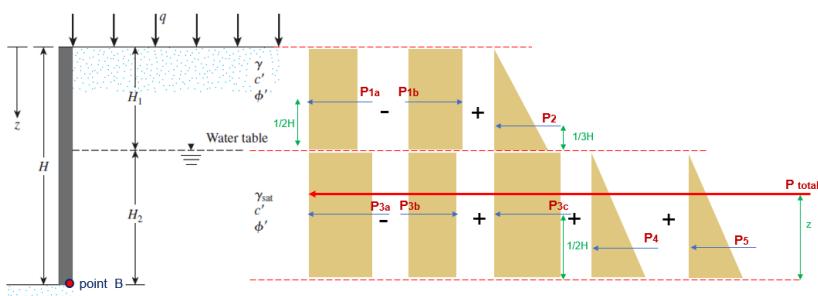
# Lateral Active Earth Pressure



For summation of the horizontal force :  $P_{\text{total}} = A_{1ab} + A_2 + A_{3abc} + A_4 + A_5$

Summing the moment of all the force about point B  $(P_{\text{total}}) \times Z = P_{1ab} + P_2 + P_{3abc} + P_4 + P_5$

# Lateral Active Earth Pressure



For summation of the horizontal force :

$$P_{\text{total}} = A_{1ab} + A_2 + A_{3abc} + A_4 + A_5$$

$$\begin{aligned} P_{\text{total}} = & H_1 \cdot (k_{a1} \cdot q - 2c_1 \sqrt{k_{a1}}) \\ & + \frac{1}{2} H_1 \cdot (K_{a1} \cdot \gamma_1 \cdot H_1) \\ & + H_2 \cdot (k_{a2} \cdot q - 2c_2 \sqrt{k_{a2}} + K_{a2} \cdot \gamma_1 \cdot H_1) \\ & + \frac{1}{2} H_2 \cdot (K_{a2} \cdot \gamma_2 \cdot H_2) + \frac{1}{2} H_2 \cdot (\gamma_w \cdot H_2) \end{aligned}$$

The distance of the line of action of the resultant force from the bottom of the wall can be determined by taking the moments about the bottom of the wall (point B) and is

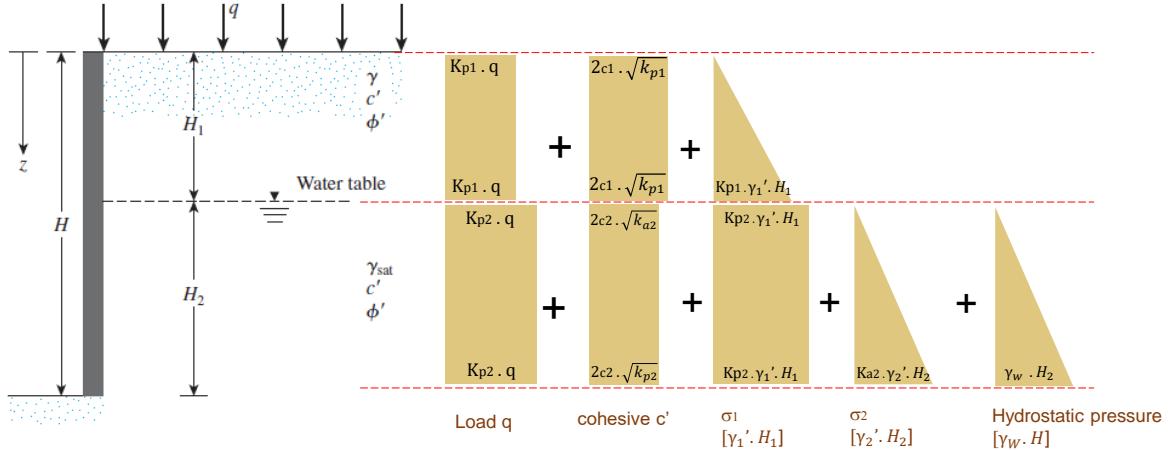
$$(P_{\text{total}}) \cdot z = [(\frac{1}{2} H_1 + H_2) \cdot (A_{1ab})] + [(1/3 H_1 + H_2) \cdot (A_2) + (\frac{1}{2} H_2) \cdot (A_{3abc})] + [(1/3 H_2) (A_4) + (1/3 H_2) \cdot (A_5)]$$

So the distance of resultant force from B is

$$Z = \frac{[(\frac{1}{2} H_1 + H_2) \cdot (A_{1ab})] + [(1/3 H_1 + H_2) \cdot (A_2) + (\frac{1}{2} H_2) \cdot (A_{3abc})] + [(1/3 H_2) (A_4) + (1/3 H_2) \cdot (A_5)]}{P_{\text{total}}}$$

# Lateral Passive Earth Pressure

**Passive Earth Pressure**  $K_p = \tan^2 \left( 45 + \frac{\phi'}{2} \right)$

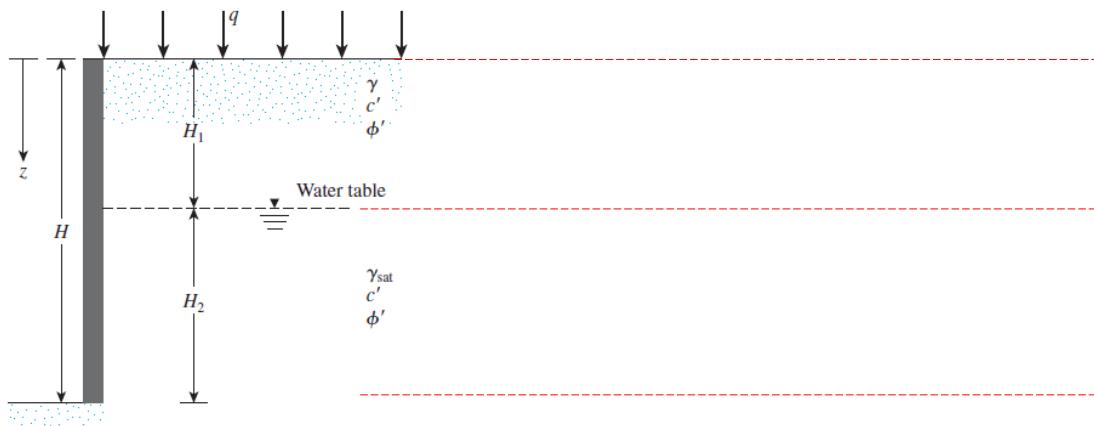


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## Problem No 2

In figure 2, let  $H_1 = 3, 4, 5$  m,  $H_2 = 3, 4, 5$  m.  $\gamma_1 = 16, 17, 18$  kN/m<sup>3</sup>,  $q = 0$ ,  $\phi'_1 = 33^\circ, 34^\circ, 35^\circ$ ,  $c'_1 = 0$ ,  $\gamma_2 = 16.5, 17.5, 18.5$  kN/m<sup>3</sup>,  $\phi'_2 = 24^\circ, 25^\circ, 26^\circ$ ,  $c'_2 = 10, 12.5, 15$  kN/m<sup>2</sup>. Determine the Rankine active force per unit length of the wall.

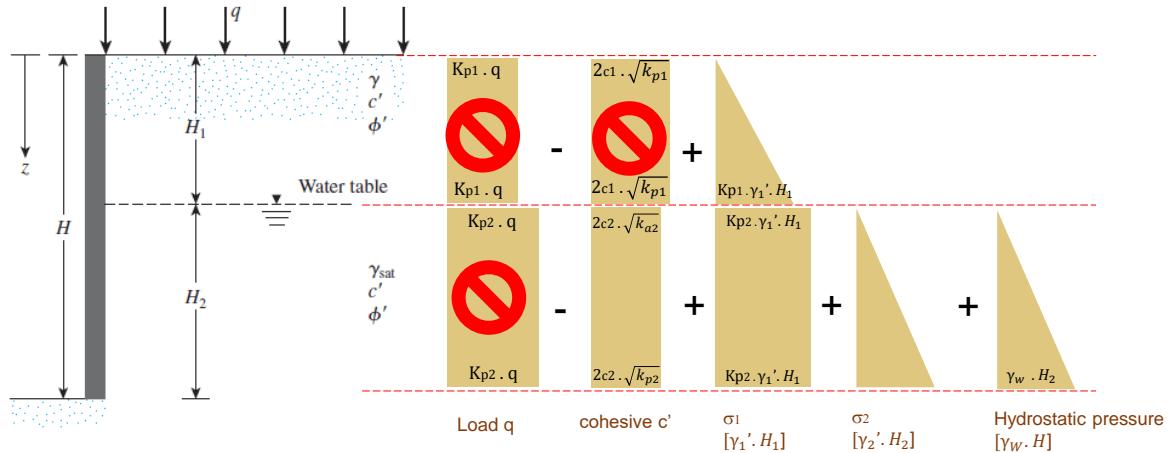


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