

# Permeability

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## Soil Mechanic I

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# Tujuan Pembelajaran

Penting untuk mengetahui kuantitas rembesan air dalam tanah pada berbagai kondisi hidraulik tanah untuk beberapa penerapan dalam pekerjaan Teknik sipil :

1. Kebutuhan alat pompa air pada konstruksi
2. Analisis kestabilan struktur bending dan bendungan
3. Analisis kestabilan struktur dinding penahan akibat adanya gaya rembesan

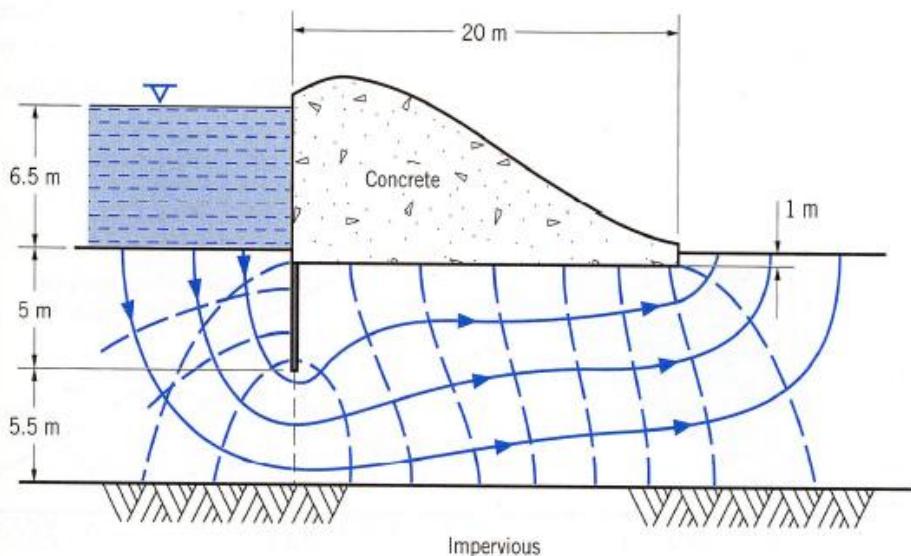


Figure 7.10 Flow net for a concrete dam with cutoff wall.

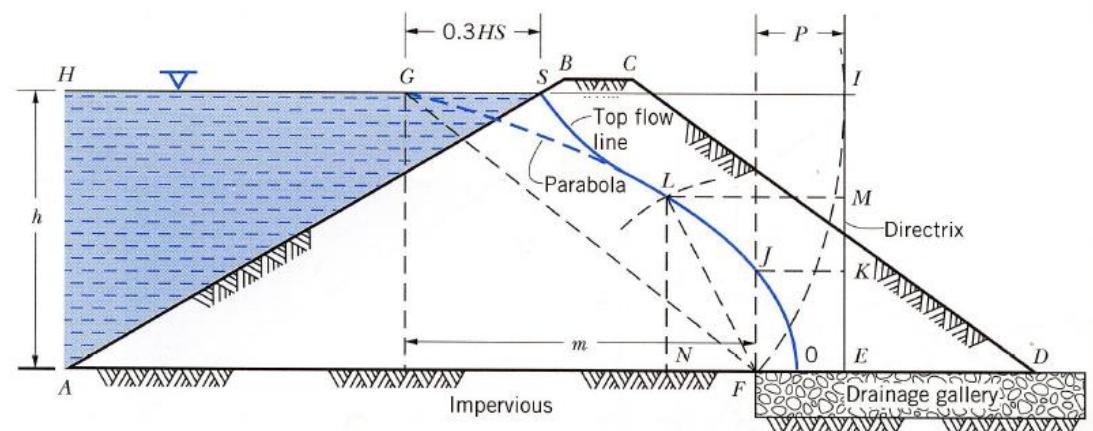
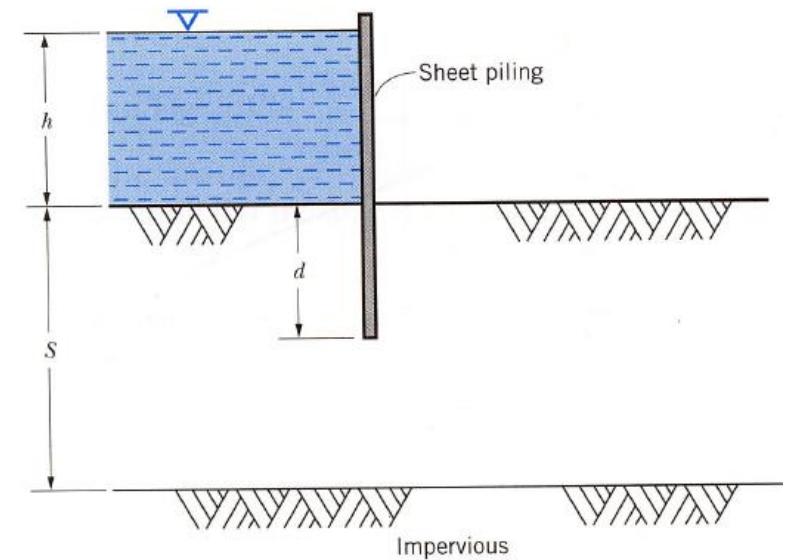


Figure 7.14 Development of top flow line from parabola.

# Rumus Bernoulli

$$h = \frac{u}{\gamma_w} + \frac{v^2}{2g} + z$$

↑              ↑              ↑  
Pressure   Velocity   Elevation  
head          head          head

where  $h$  = total head  
 $u$  = pressure  
 $v$  = velocity  
 $g$  = acceleration due to gravity  
 $\gamma_w$  = unit weight of water

Air mengalir dari energi yang tinggi menuju energi yang rendah. Berdasarkan rumus Bernoulli, Total head adalah penjumlahan dari pressure head, velocity head, dan elevasi head.

Air yang mengalir melalui pori-pori tanah. Untuk menghitung besar perbedaan energi dari suatu titik datum. Kecepatan aliran air sangat kecil sehingga nilai velocity head bisa diabaikan pada perhitungan ini

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Pressure   Velocity   Elevation  
head          head          head

$$h = \frac{u}{\gamma_w} + Z$$

# Rumus Bernoulli

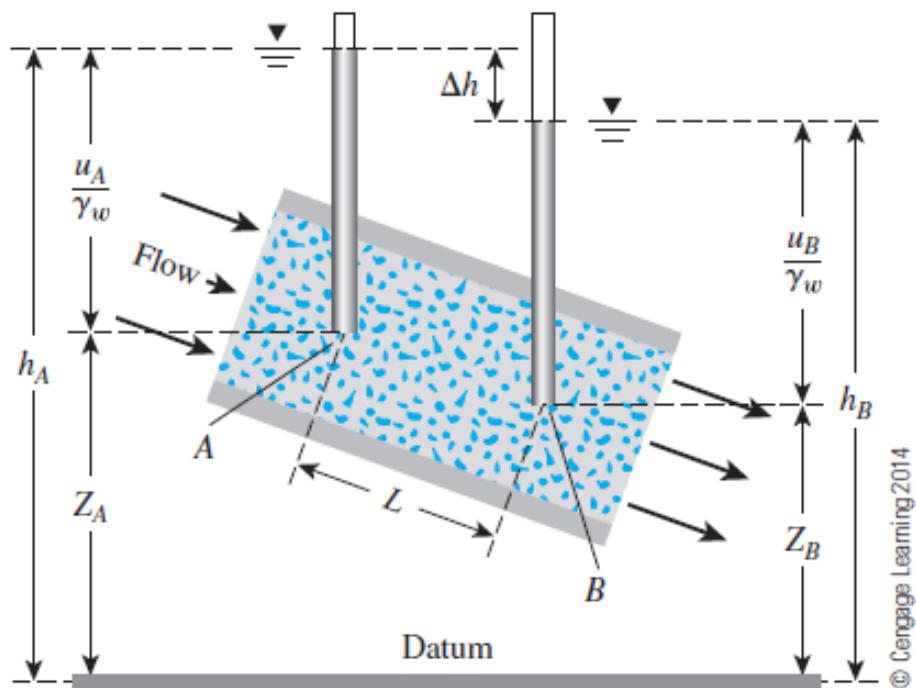


Figure 7.1 Pressure, elevation, and total heads for flow of water through soil

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$$\Delta h = \Delta he + \Delta hp$$

$\Delta h$  = selisih perbedaan energi total head

$\Delta he$  = selisih perbedaan elevasi

$\Delta hp$  = selisih perbedaan tekanan

$$hp = \frac{u}{\gamma_w}$$
$$he = Z$$

$$h = \frac{u}{\gamma_w} + Z$$

# Rumus Bernoulli

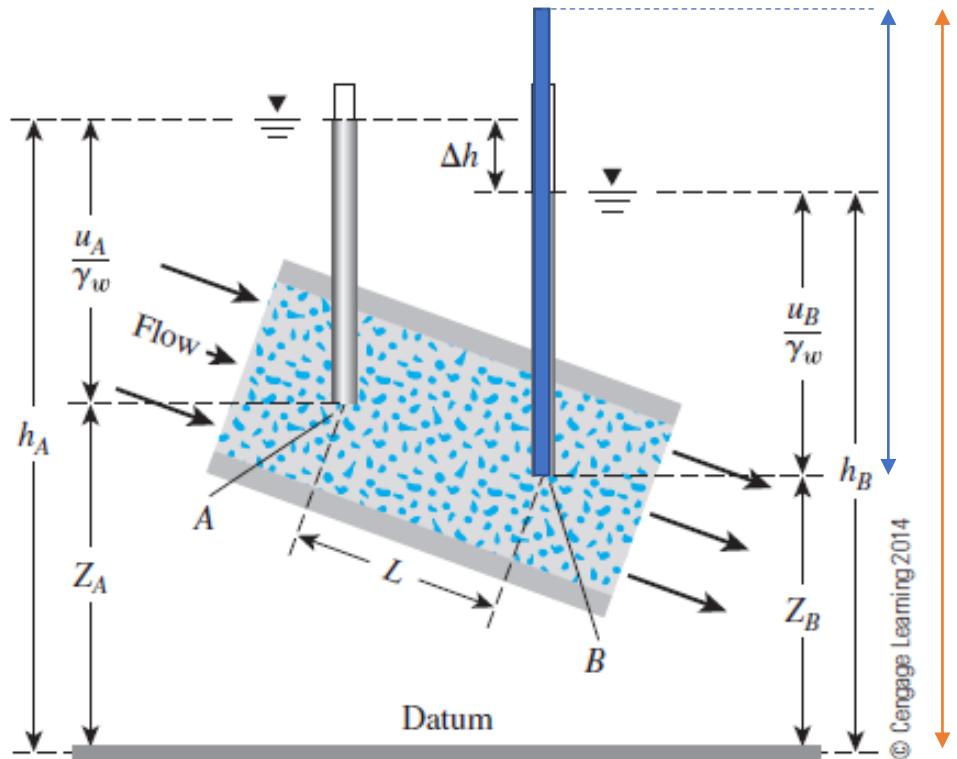


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# Rumus Bernoulli

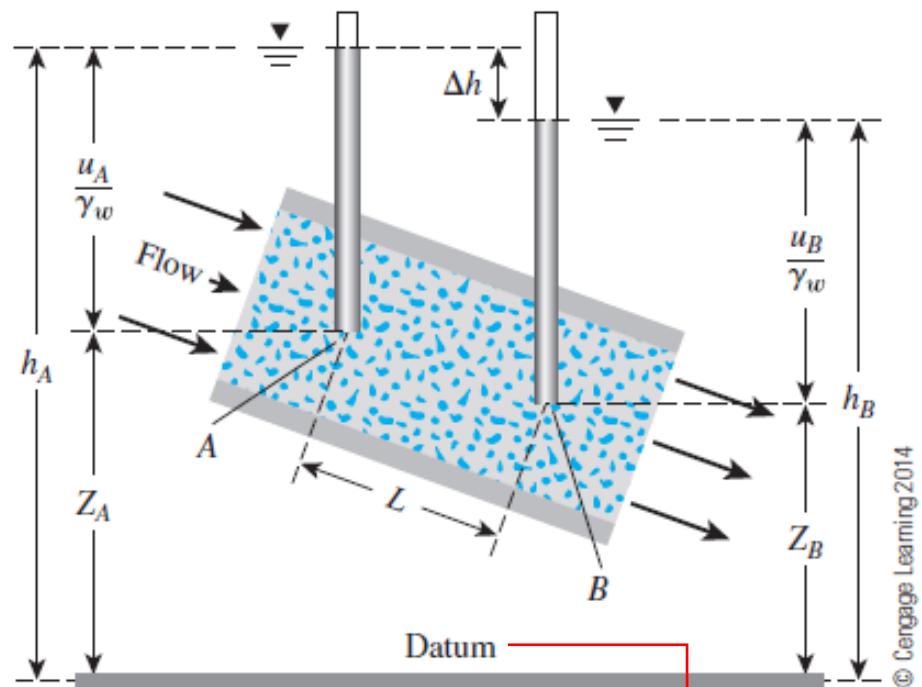


Figure 7.1 Pressure, elevation, and total heads for flow of water through soil

→ Lokasi Datum  
diasumsikan

$$\Delta h = hA - hB$$

$$hA = hpA + heA$$

$$hB = hpB + heB$$

$$hA = \frac{uA}{\gamma w} + Z_A$$

$$hB = \frac{uB}{\gamma w} + Z_B$$

$$h = \frac{u}{\gamma w} + Z$$

$$hp = \frac{u}{\gamma w}$$

$$he = Z$$

# Contoh

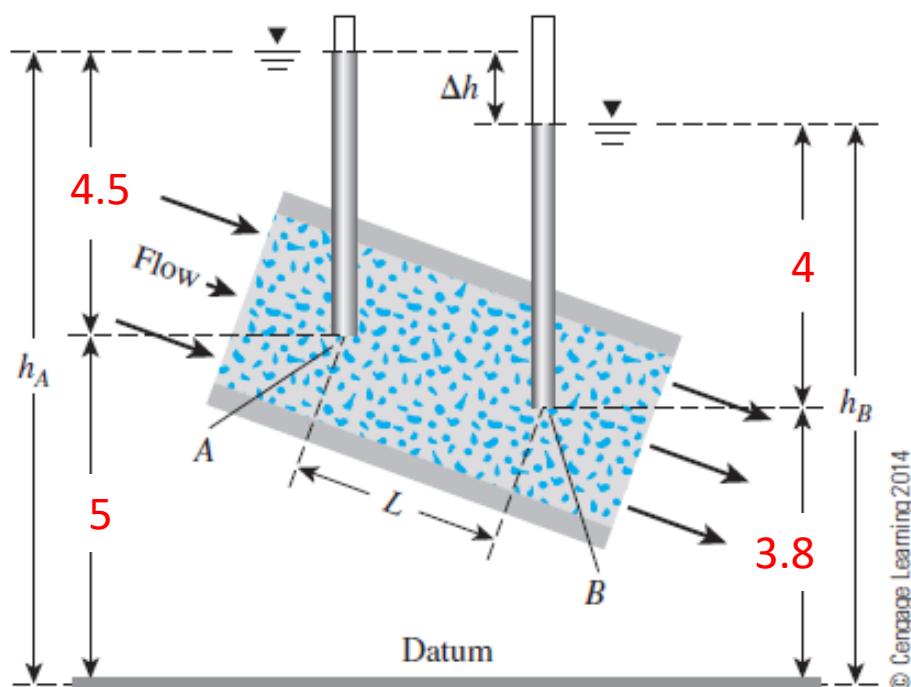


Figure 7.1 Pressure, elevation, and total heads for flow of water through soil

Perbedaan total Head dari titik A ke titik B

$$\Delta h = hA - hB$$

$$hA = hpA + heA$$

$$hA = 4.5 + 5 = 9.5$$

$$hB = hpB + heB$$

$$hB = 4 + 3.8 = 7.8$$

$$\Delta h = 9.5 - 7.8 = 1.7m$$

Terdapat perbedaan tinggi total head sebesar 1.7 m. air mengalir dari titik A menuju titik B

# Contoh

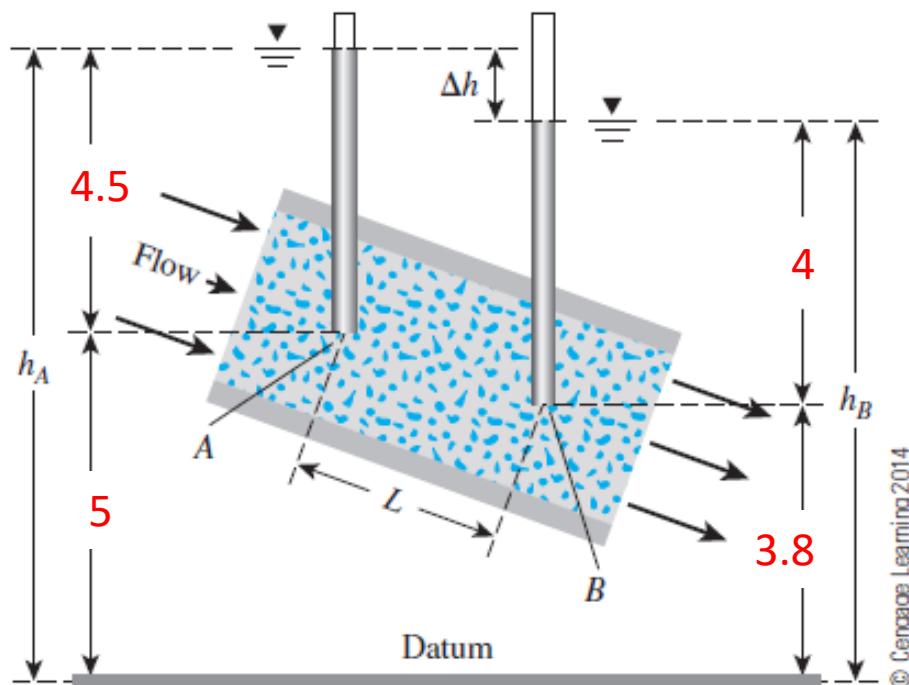


Figure 7.1 Pressure, elevation, and total heads for flow of water through soil

Perbedaan total Head dari titik A ke titik B

$\Delta h$  dapat disebut juga kehilangan energi.  
Dapat dihitung dengan rumus berikut :

$$i = \frac{\Delta h}{L}$$

$i$  = gradien hidraulik

$L$  = jarak antara titik A ke B, atau Panjang aliran dimana kehilangan energi terjadi

# Hukum Darcy

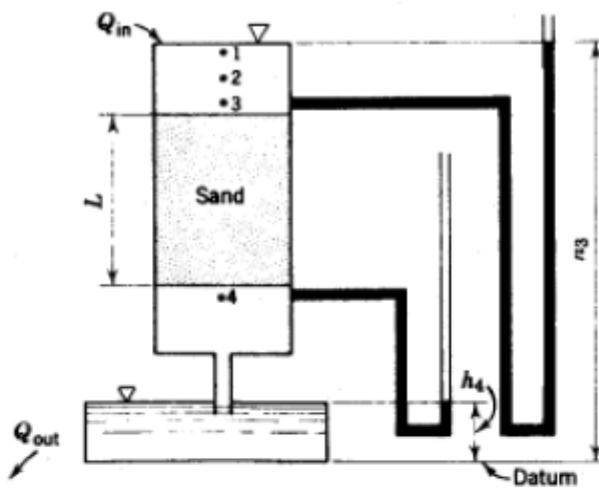
$$v = ki \quad (7.6)$$

where  $v$  = *discharge velocity*, which is the quantity of water flowing in unit time through a unit gross cross-sectional area of soil at right angles to the direction of flow  
 $k$  = hydraulic conductivity (otherwise known as the coefficient of permeability)

$$q = vA = A_v v_s$$

where  $v_s$  = seepage velocity  
 $A_v$  = area of void in the cross section of the specimen

# Hukum Darcy



## ■ Persamaan Darcy:

$$Q = k \frac{h_3 - h_4}{L} A = k i A$$

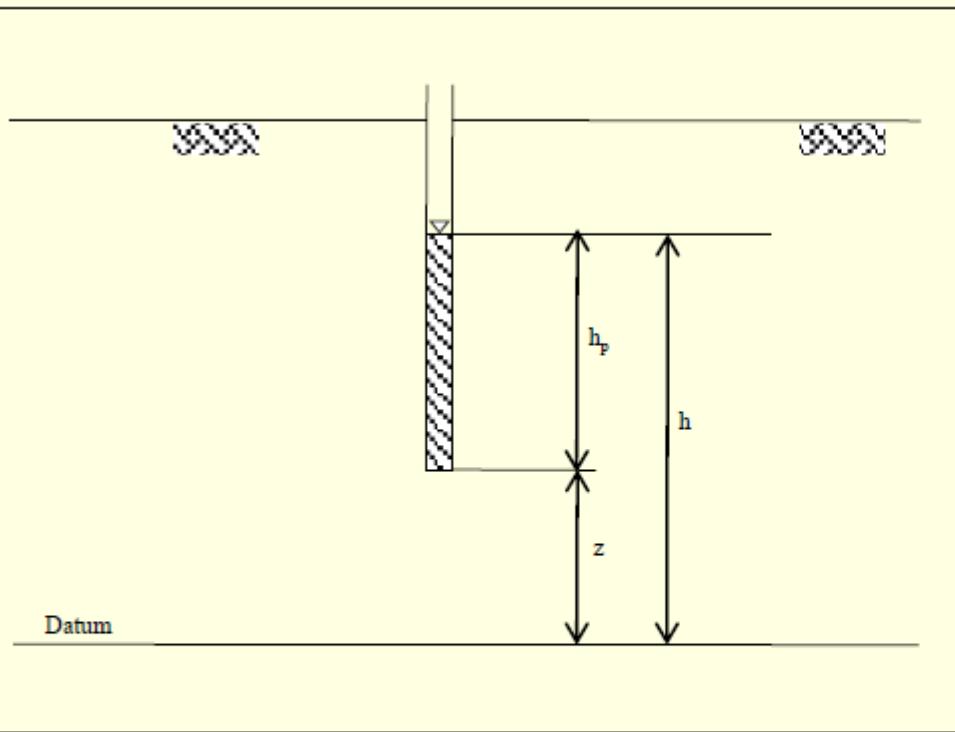
$$Q = v A \quad \text{dengan} \quad v = k \frac{h_3 - h_4}{L} = k i$$

## ■ Dimana:

$v$  = kecepatan pengaliran,

$i$  = hydraulic gradient

# Hukum Darcy



$$h = h_p + h_e + h_v = \text{constant}$$

di mana:

- $h$  = *total head*,
- $h_p = \frac{u}{\gamma_w}$  = *pressure head*,
- $h_e = z$  = *elevation head*,
- $h_v = \frac{v^2}{2g}$  = *velocity head*,
- $u$  = tekanan air pori,
- $z$  = elevasi dari suatu titik terhadap suatu datum,
- $v$  = kecepatan pengaliran, dan
- $g$  = percepatan gravitasi.

# Uji Permeabilitas di laboratorium

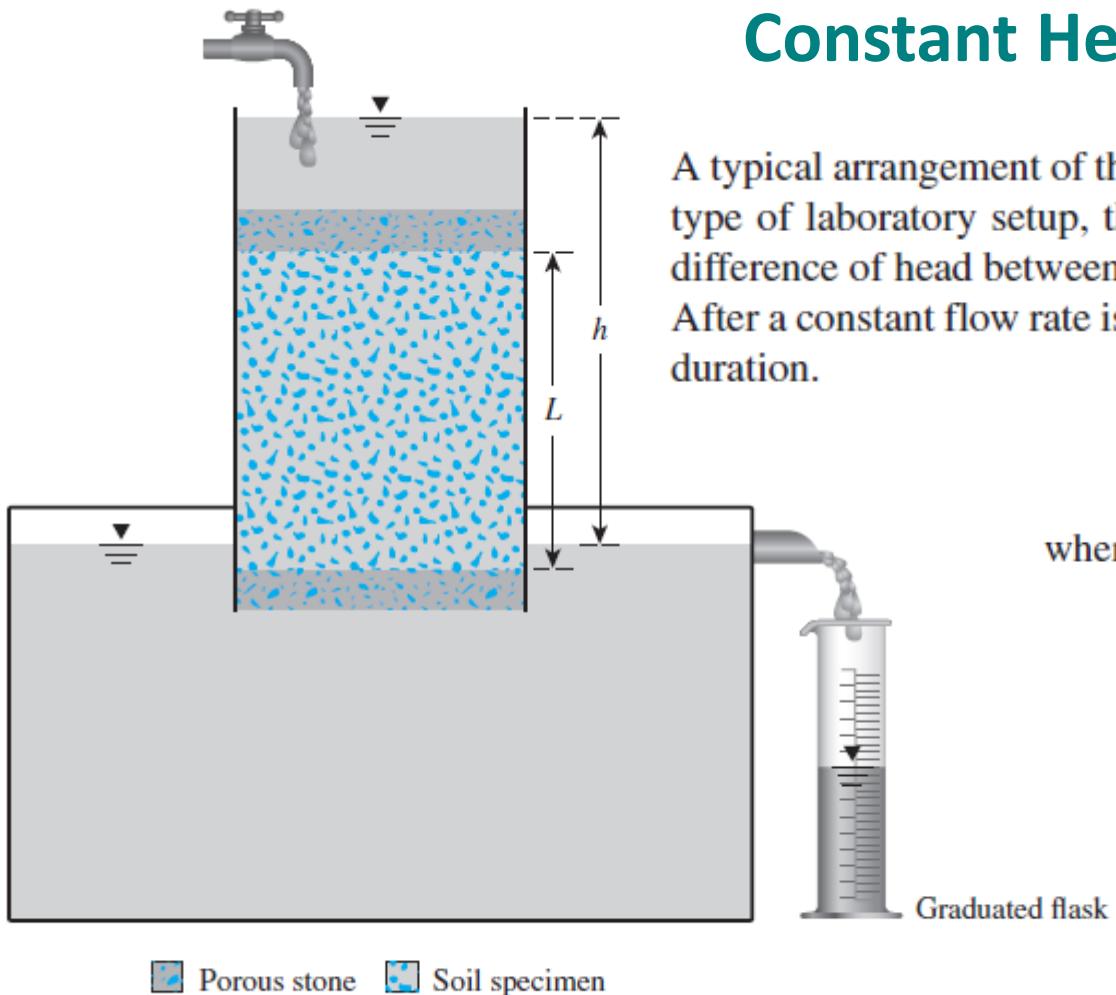


Figure 7.5 Constant-head permeability test

## Constant Head Test

A typical arrangement of the constant-head permeability test is shown in Figure 7.5. In this type of laboratory setup, the water supply at the inlet is adjusted in such a way that the difference of head between the inlet and the outlet remains constant during the test period. After a constant flow rate is established, water is collected in a graduated flask for a known duration.

The total volume of water collected may be expressed as

$$Q = Avt = A(ki)t$$

where  $Q$  = volume of water collected

$A$  = area of cross section of the soil specimen

$t$  = duration of water collection

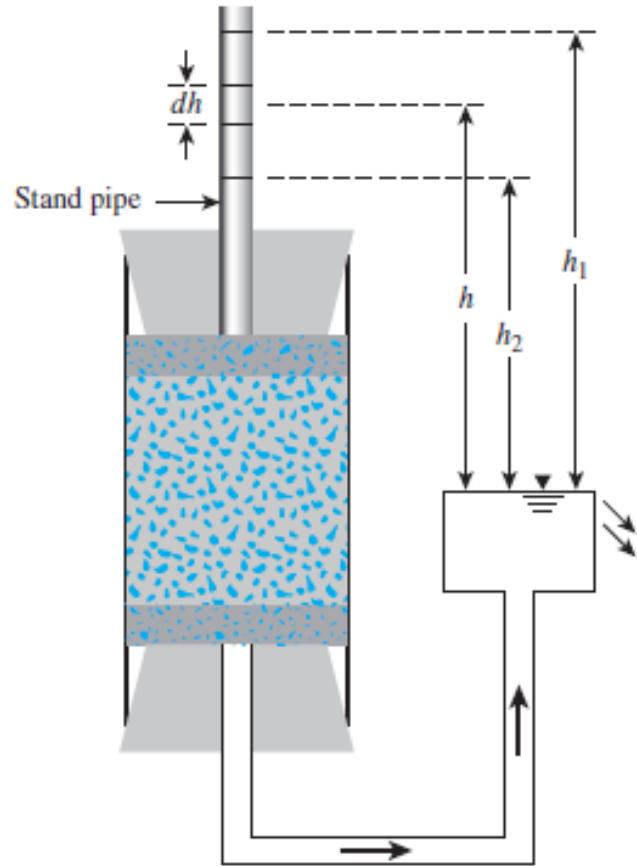
$$i = \frac{h}{L} \quad \text{where } L = \text{length of the specimen,}$$

$$Q = A \left( k \frac{h}{L} \right) t \quad k = \frac{QL}{Aht}$$

a constant-head test arrangement in the laboratory for a test on a granular soil.

# Uji Permeabilitas di laboratorium

## Falling - Head Test



A typical arrangement of the falling-head permeability test is shown in Figure. Water from a standpipe flows through the soil. The initial head difference  $h_1$  at time  $t=0$  is recorded, and water is allowed to flow through the soil specimen such that the final head difference at time  $t = t_2$  is  $h_2$ .

$$q = k \frac{h}{L} A$$

where  $q$  = flow rate

$a$  = cross-sectional area of the standpipe

$A$  = cross-sectional area of the soil specimen

$$k = 2.303 \frac{aL}{At} \log_{10} \frac{h_1}{h_2}$$

Porous stone   Soil specimen

# Contoh

## Constant Head Test

- $L = 30 \text{ cm}$
- $A = \text{area of the specimen} = 177 \text{ cm}^2$
- Constant-head difference,  $h = 50 \text{ cm}$
- Water collected in a period of 5 min =  $350 \text{ cm}^3$

Calculate the hydraulic conductivity in cm/sec.

$$k = \frac{QL}{Aht}$$

Given  $Q = 350 \text{ cm}^3$ ,  $L = 30 \text{ cm}$ ,  $A = 177 \text{ cm}^2$ ,  $h = 50 \text{ cm}$ , and  $t = 5 \text{ min}$ , we have

$$k = \frac{(350)(30)}{(177)(50)(5)(60)} = 3.95 \times 10^{-3} \text{ cm/sec}$$

## Falling - Head Test

For a falling-head permeability test, the following values are given:

- Length of specimen = 200 mm.
- Area of soil specimen =  $1000 \text{ mm}^2$ .
- Area of standpipe =  $40 \text{ mm}^2$ .
- Head difference at time  $t = 0 = 500 \text{ mm}$ .
- Head difference at time  $t = 180 \text{ sec} = 300 \text{ mm}$ .

Determine the hydraulic conductivity of the soil in cm/sec.

$$k = 2.303 \frac{aL}{At} \log_{10} \left( \frac{h_1}{h_2} \right)$$

We are given  $a = 40 \text{ mm}^2$ ,  $L = 200 \text{ mm}$ ,  $A = 1000 \text{ mm}^2$ ,  $t = 180 \text{ sec}$ ,  $h_1 = 500 \text{ mm}$ , and  $h_2 = 300 \text{ mm}$ ,

$$\begin{aligned} k &= 2.303 \frac{(40)(200)}{(1000)(180)} \log_{10} \left( \frac{500}{300} \right) \\ &= 2.27 \times 10^{-2} \text{ cm/sec} \end{aligned}$$

# note

Nilai **k** sering disebut sebagai koefisien permeabilitas atau konduktivitas hidraulik  
**k** dibuat dalam satuan panjang per waktu

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Rentang nilai koefisien permabilitas (k) berdasarkan tipe tanah

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Soil type	<i>k</i> cm/sec
Clean gravel	100–1.0
Coarse sand	1.0–0.01
Fine sand	0.01–0.001
Silty clay	0.001–0.00001
Clay	<0.000001

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## Rasio nilai koefisien permeabilitas arah horizontal dan vertikal

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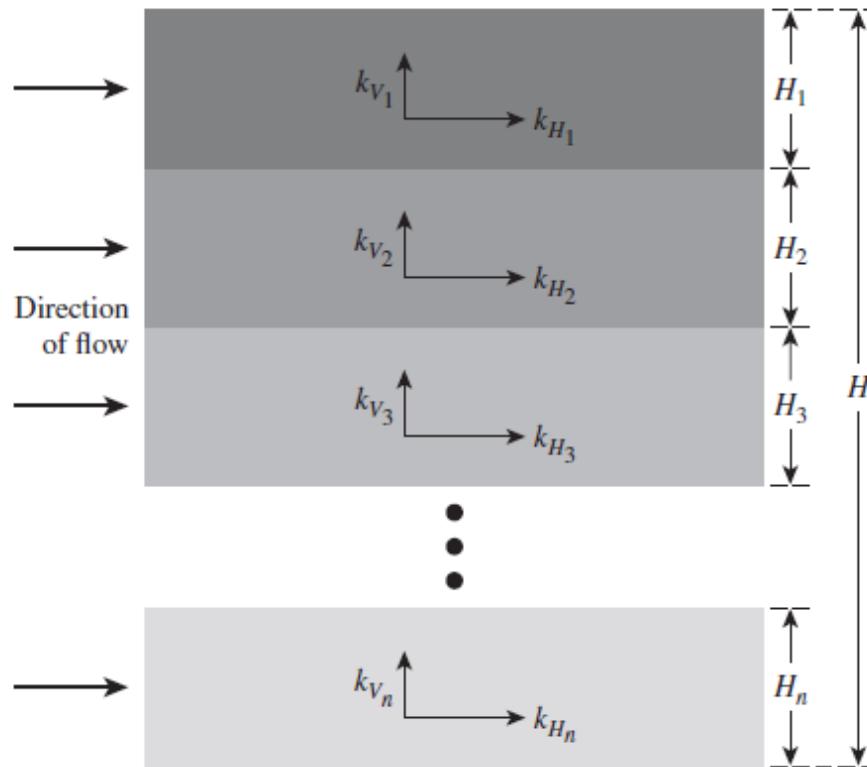
Soil type	$k_H/k_V$	Reference
Organic silt with peat	1.2 to 1.7	Tsien (1955)
Plastic marine clay	1.2	Lumb and Holt (1968)
Soft clay	1.5	Basett and Brodie (1961)
Varved clay	1.5 to 1.7	Chan and Kenney (1973)
Varved clay	1.5	Kenney and Chan (1973)
Varved clay	3 to 15	Wu et al. (1978)
Varved clay	4 to 40	Casagrande and Poulos (1969)

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Most soils are not isotropic with respect to permeability. In a given soil deposit, the magnitude of  $k$  changes with respect to the direction of flow. Figure 7.19 shows a soil layer through which water flows in a direction inclined at an angle  $\alpha$  with the vertical. Let the hydraulic conductivity in the vertical ( $\alpha = 0$ ) and horizontal ( $\alpha = 90^\circ$ ) directions be  $k_V$  and  $k_H$ , respectively. The magnitudes of  $k_V$  and  $k_H$  in a given soil depend on several factors, including the method of deposition in the field.

# note

In a stratified soil deposit where the hydraulic conductivity for flow in a given direction changes from layer to layer, an equivalent hydraulic conductivity can be computed to simplify calculations. The following derivations relate to the equivalent hydraulic conductivities for flow in vertical and horizontal directions through multilayered soils with horizontal stratification.



$$k_{H(\text{eq})} = \frac{1}{H} (k_{H_1}H_1 + k_{H_2}H_2 + k_{H_3}H_3 + \dots + k_{H_n}H_n)$$

$$k_{v(\text{eq})} = \frac{H}{\left(\frac{H_1}{k_{V_1}}\right) + \left(\frac{H_2}{k_{V_2}}\right) + \left(\frac{H_3}{k_{V_3}}\right) + \dots + \left(\frac{H_n}{k_{V_n}}\right)}$$

# Seepage

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## Soil Mechanic I

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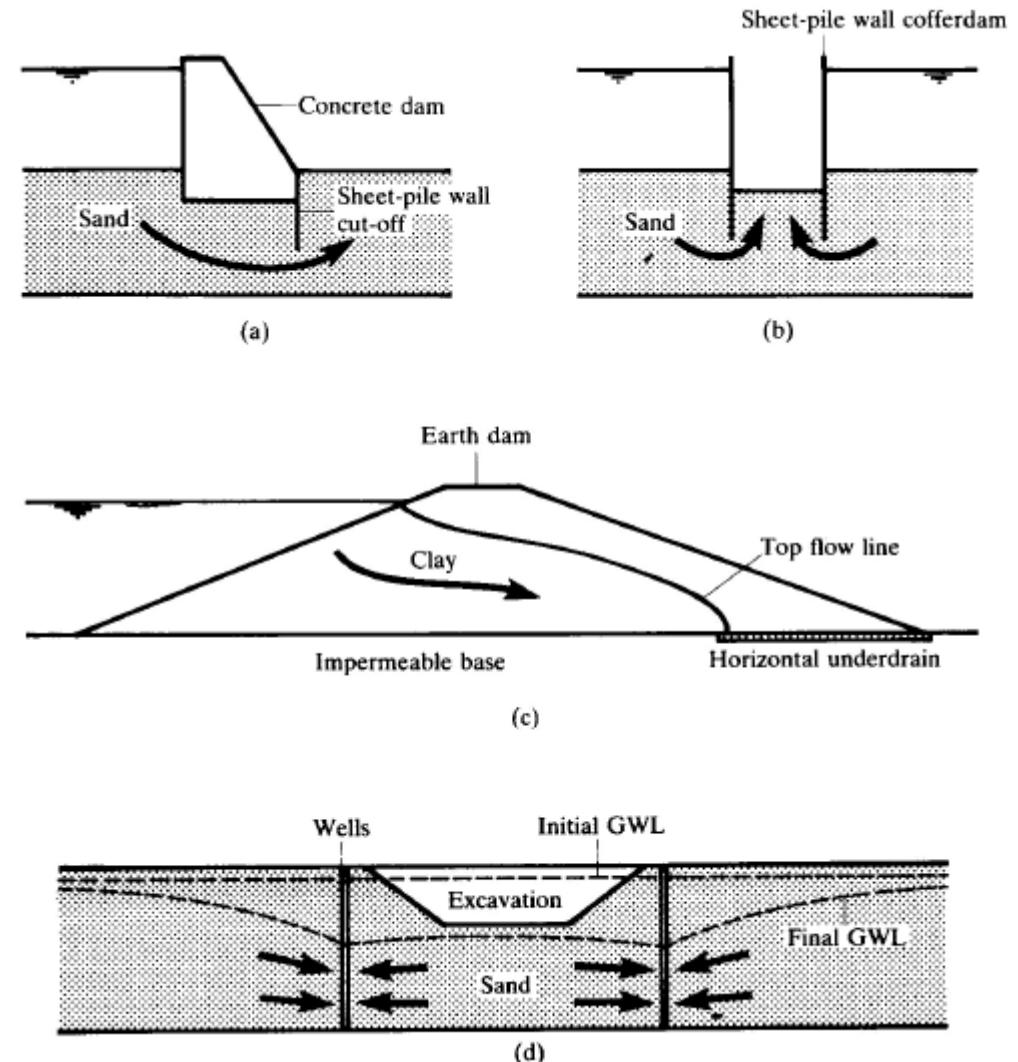


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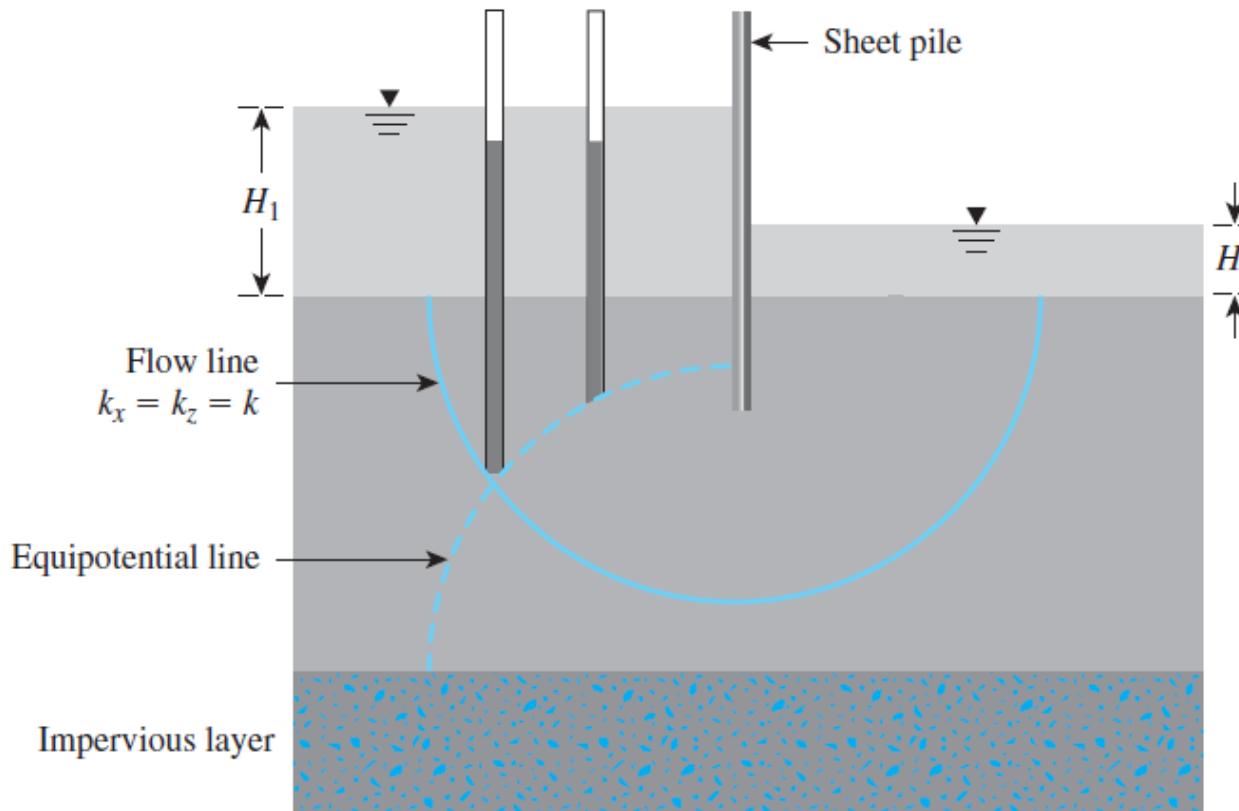
# Tujuan Pembelajaran

Dapat menghitung besarnya rembesan dalam tanah dan menetukan tekanan uplift yang terjadi pada bangunan air.

Seepage (Rembesan) : untuk mengetahui jumlah rembesan air yang mengalir pada tanah, baik dibawah dinding penahan (sheet pile) atau pun yang melewati pada tubuh bendungan.



# Flownet



Flow line : Garis aliran rembesan

Equipotential line : garis dengan potential head yang sama

# Flownet

Sekumpulan *flow lines & equipotential line*, menurut Darcy :

$$\Delta q = A \cdot v = A \cdot k \cdot i = (a \cdot 1) k \cdot \frac{\Delta h}{b}$$

$$\Delta q = \frac{a}{b} \cdot k \cdot \Delta h$$

diasumsikan  $a=b$

Dimana : Nd = Equipotential drop

$$\Delta h = \frac{h_1 - h_2}{Nd} = \frac{\Delta H}{Nd}$$

$$\Delta H = h_1 - h_2$$

Sehingga Debit per satuan panjang adalah

$$\Delta q = \frac{a}{b} \cdot k \cdot \frac{h_1 - h_2}{Nd}$$

$$\Delta q = k \cdot \frac{\Delta H}{Nd}$$

# Flownet

## Debit Total

Dimana : Nd = Equipotential drop

Total Flow-nya menjadi :

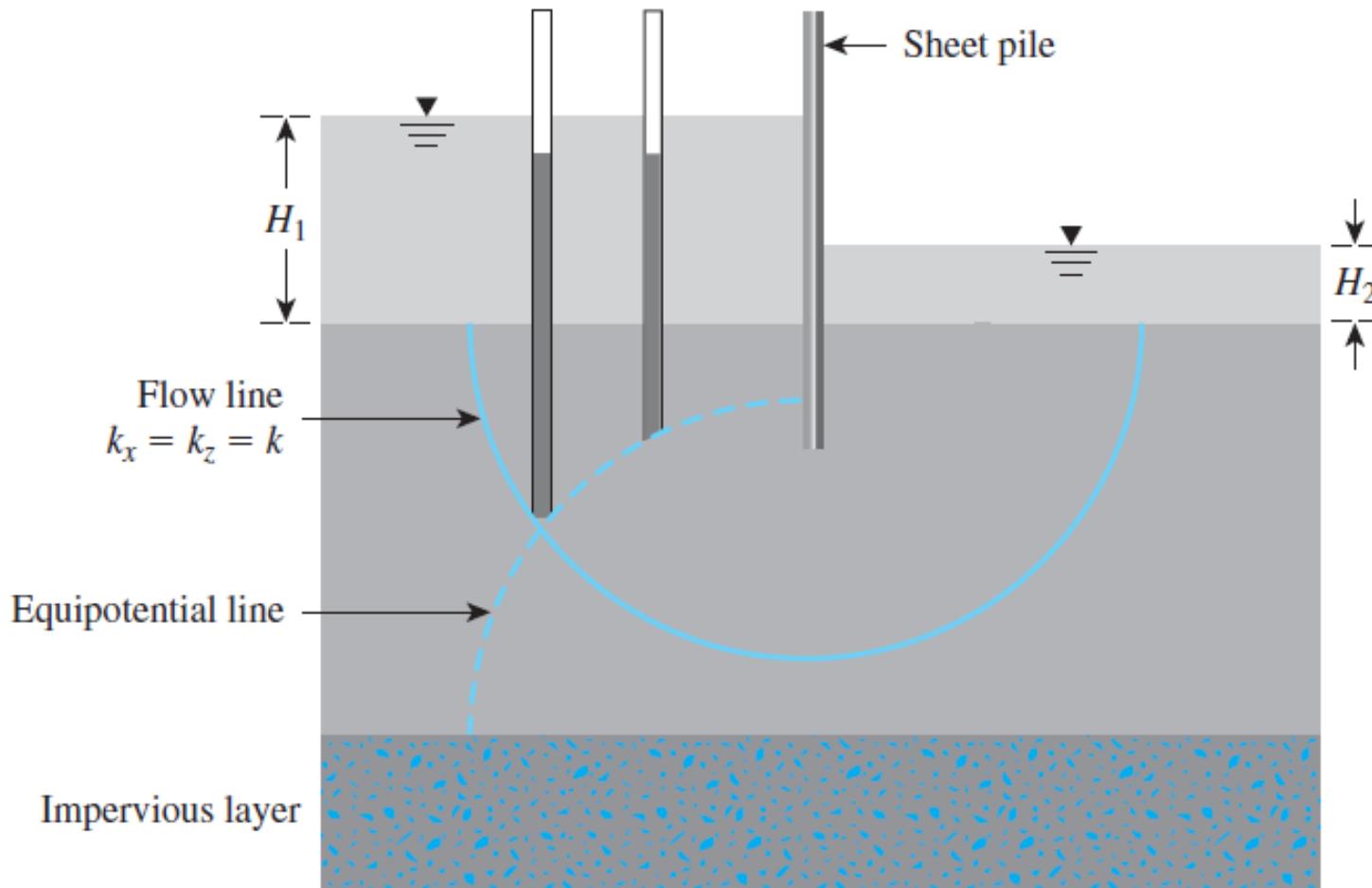
$$q = \Sigma \Delta q = Nf \cdot k \cdot \left[ \frac{a}{b} \right] \left[ \frac{h_1 - h_2}{Nd} \right]$$

$$q = k \left[ \frac{Nf}{Nd} \right] \Delta H \left[ \frac{a}{b} \right]$$

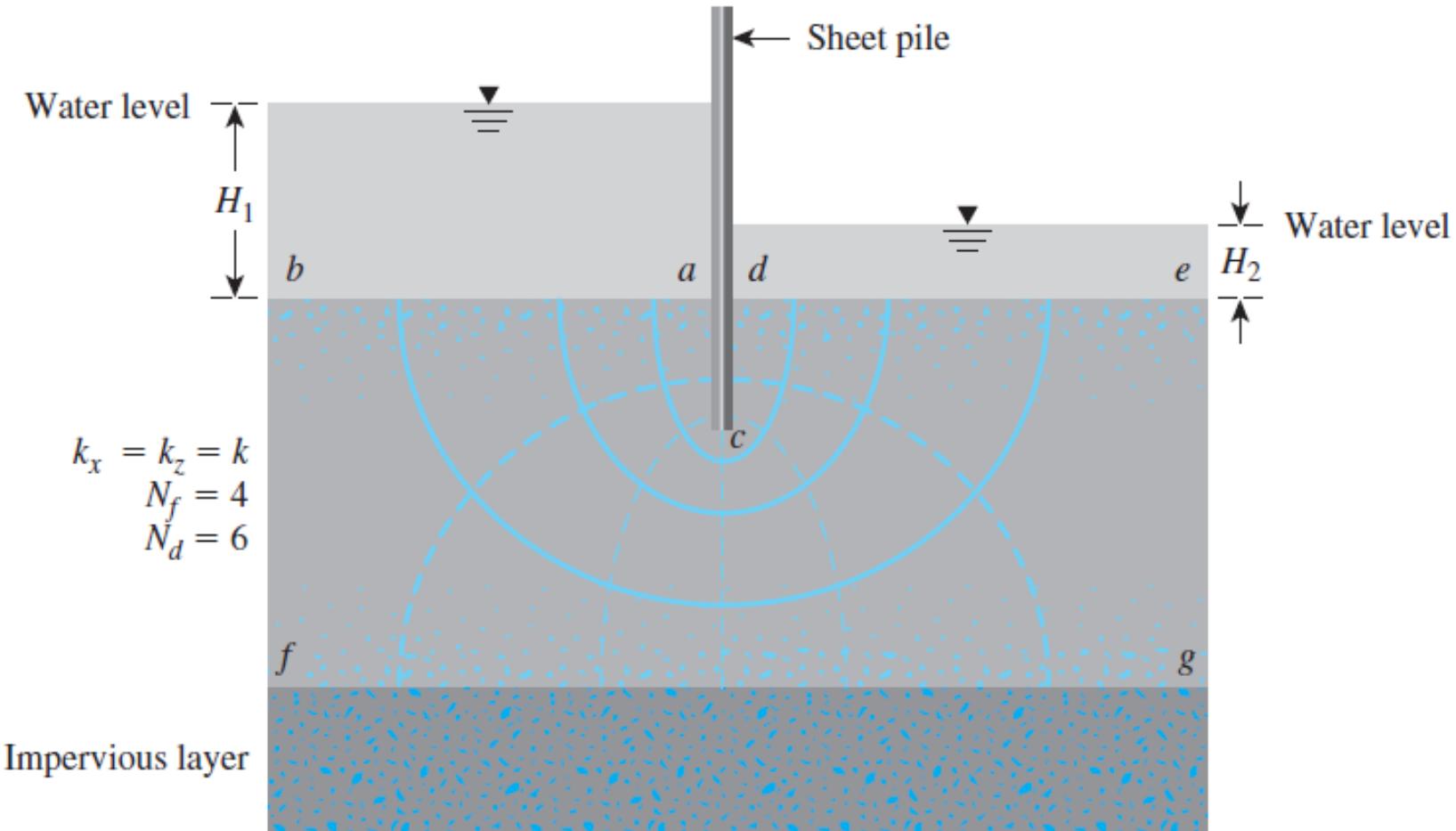
Untuk  $a = b$  persamaan menjadi :

Atau :  $q_{\text{total}} = k \left[ \frac{Nf}{Nd} \right] \Delta H \quad \Delta H = h_1 - h_2$

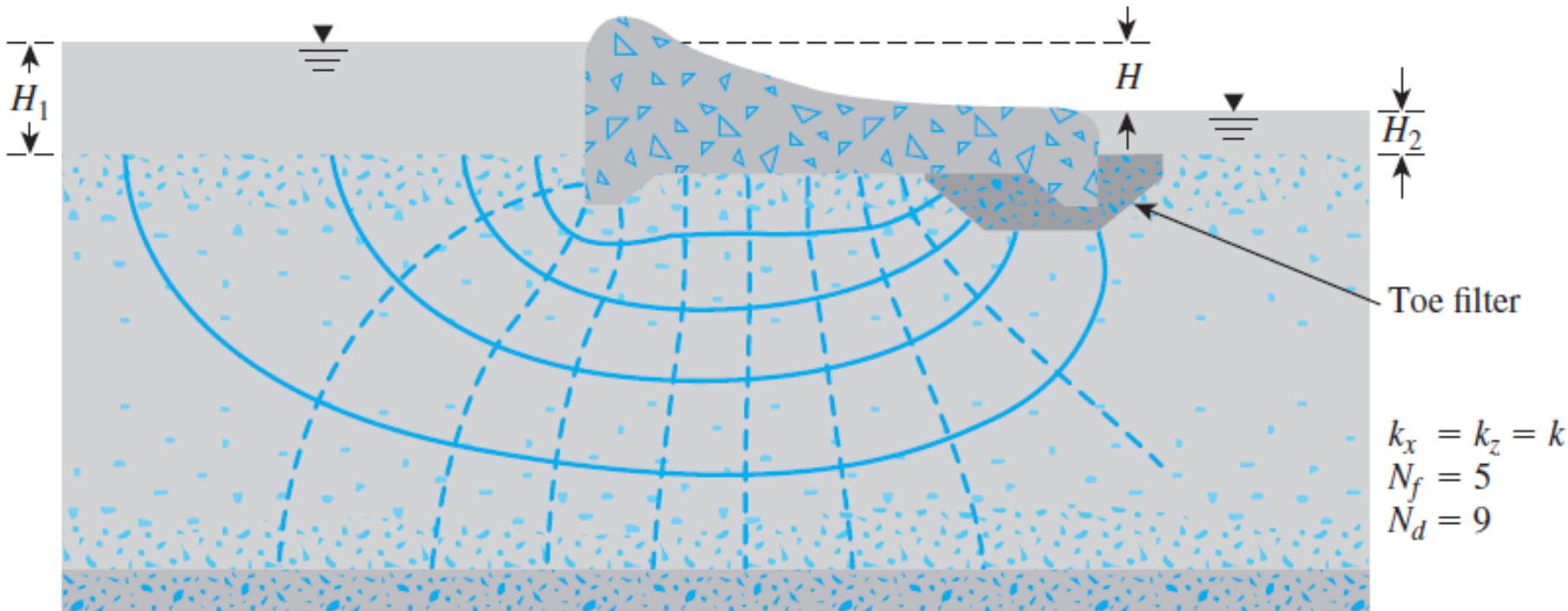
# Flownet (Contoh)



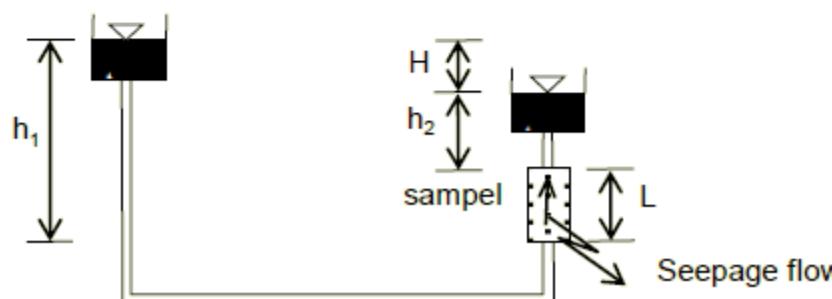
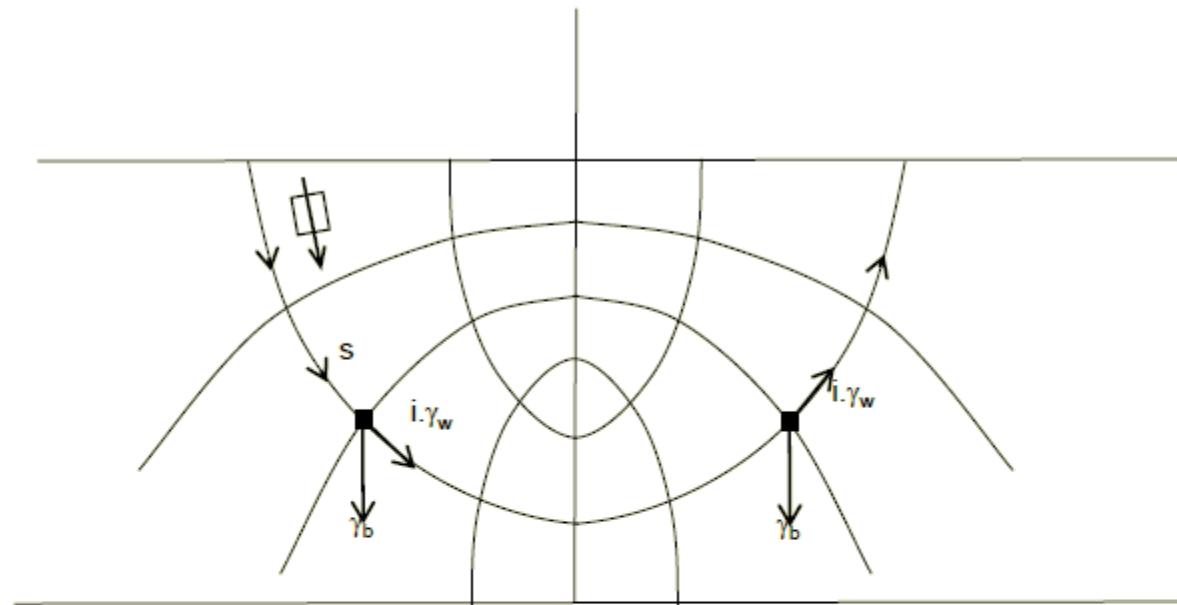
# Flownet (Contoh)



# Flownet (Contoh)



# Seepage Force

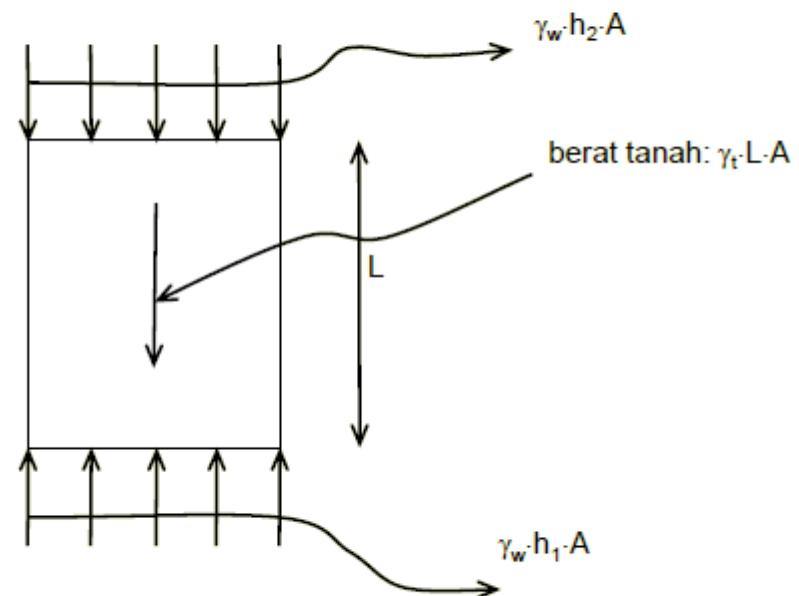


# Seepage Force

$$\text{Resultante Force} = \gamma_t L A - \gamma_w (h_1 - h_2) A$$

$$\begin{aligned} \text{Body force} &= \frac{\text{force}}{\text{volume}} \\ &= \frac{\gamma_t L A - \gamma_w (h_1 - h_2) A}{L A} \\ &= \gamma_t - \gamma_w \left( \frac{H + L}{L} \right) = \gamma_t - \gamma_w (1 + i) \\ &= \gamma_{\text{buoyant}} - i \gamma_w \end{aligned}$$

$$i_{\text{critis}} = \frac{\gamma'}{\gamma_w}$$



# Sand Boiling



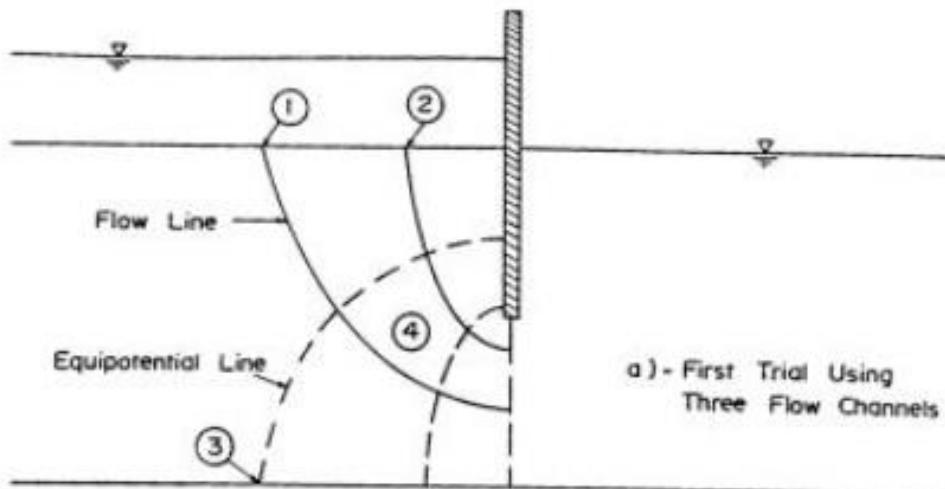
Boiling adalah aliran air (dan tanah halus) ke dasar lubang galian akibat tekanan air di luar galian yang lebih besar tekanan di dalam galian

# Sand Boiling



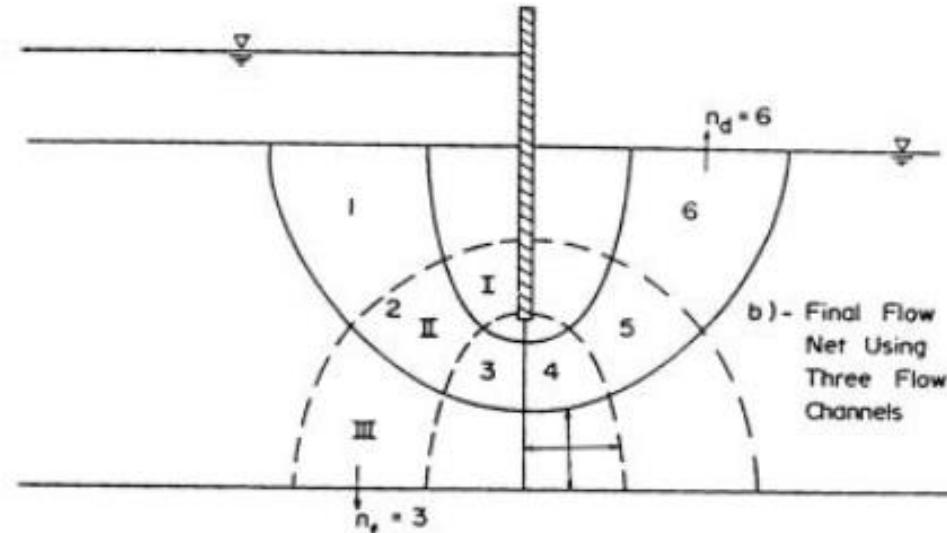
Apabila rembesan di bawah bangunan air tidak dikontrol secara sempurna, maka keadaan tersebut mengasilkan gradien hidrolik yang cukup besar di tempat keluar (bagian hilir sungai) dekat konstruksi. Gradien yang tinggi di tempat keluar tersebut berarti gaya rembes juga besar. Sehingga menyebabkan tanah menggelembung ke atas (heave) atau menyebabkan tanah kehilang kekuatannya. Keadaan ini akan mempengaruhi kestabilan bagunan air yang bersangkutan

# Flownet Construction

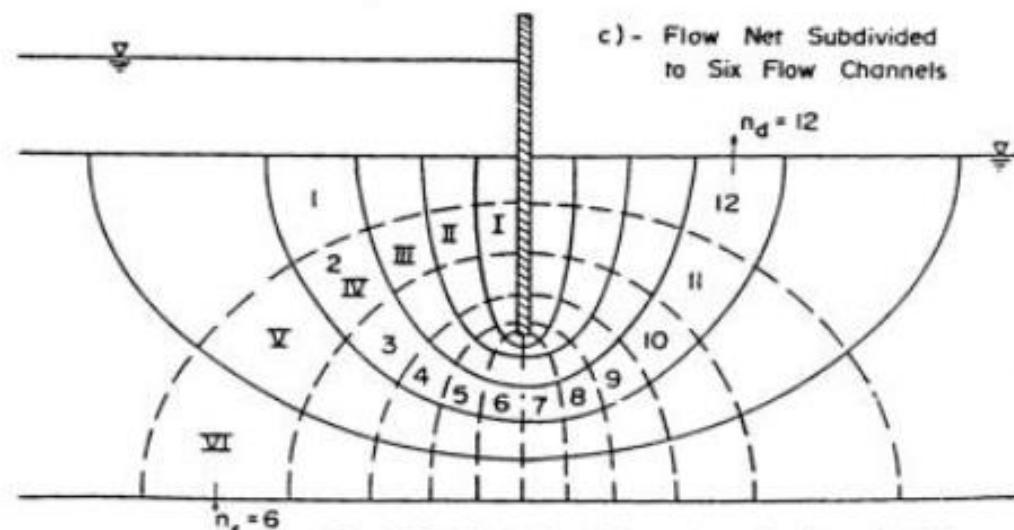


a ) - First Trial Using  
Three Flow Channels

$$\text{Transformed section : } q = k_e \frac{N_f}{N_d} \Delta H$$

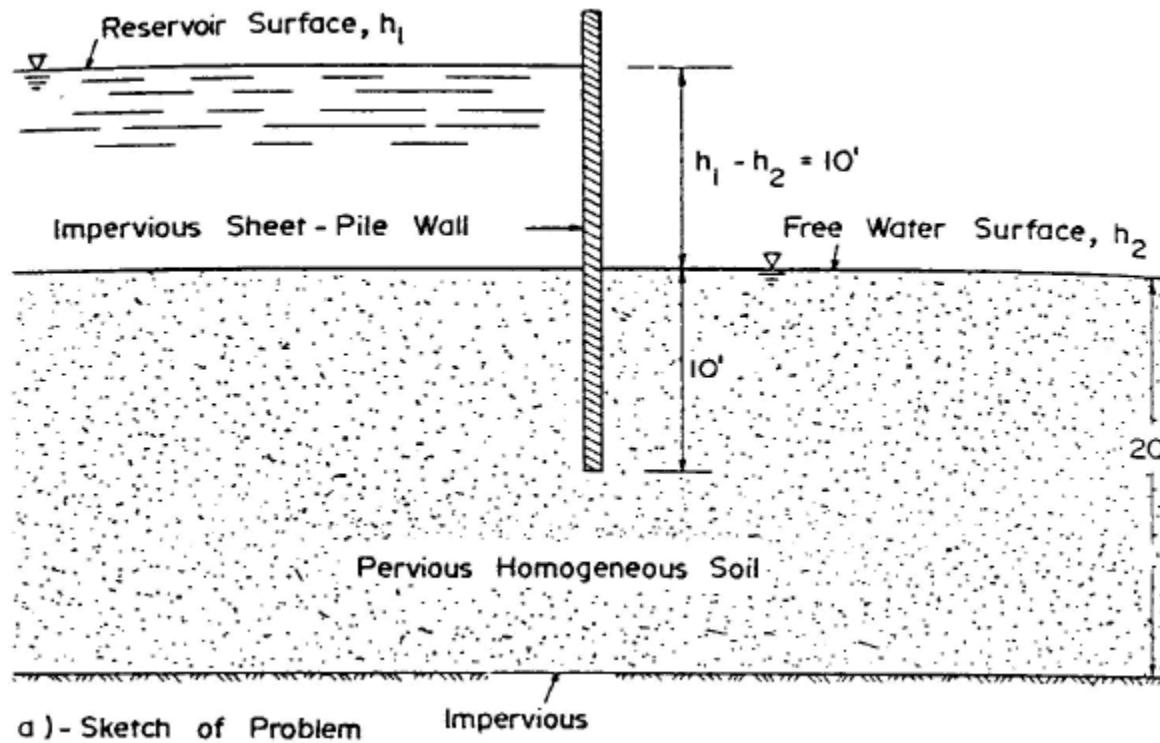


b ) - Final Flow  
Net Using  
Three Flow  
Channels



c ) - Flow Net Subdivided  
to Six Flow Channels

# Flownet Construction



# Flownet Construction

